



Numerical Solution of Natural Convection on a Vertical Stretching Surface with Suction and Blowing

Shankar Goud Bejawada^{1*}, Yanala Dharmendar Reddy², Kanti Sandeep Kumar³, Epuri Ranjith Kumar⁴

¹ Department of Mathematics, JNTUH College of Engineering Hyderabad, Kukatpally, Telangana 500085, India

² Department of Mathematics, Anurag University, Hyderabad, Telangana 500088, India

³ Department of Mathematics, Hyderabad Institute of Technology and Management, Hyderabad, Telangana 501401, India

⁴ Department of Mathematics, Kakatiya Institute of Technology and Science, Warangal 506371, Telangana, India

Corresponding Author Email: bsgoud.mtech@gmail.com

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ABSTRACT

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In this paper, the natural convective heat transfer from a stretching sheet oriented vertically involving surface mass transfer is of primary focus. A similarity solution in three dimensions is described for energy and momentum. The transformed equations are answered by using MATLAB in-built numerical programmer solver *bvp4c*. For a range of Prandtl numbers and surface mass transfer rates, friction factor and Nusselt numbers are tabulated. The heat transfer mechanism is observed to influence surface mass transfer. Heat transfer rate increases and thermal boundary layer thickness decreases with an increase of Prandtl values. In addition, the current results are compared with the previously published results and initiate to be a successful agreement.

1. INTRODUCTION

Heat transfer by natural convection frequently occurs in many physical problems and engineering applications, Viscous fluid flow studies are conducted in many practical applications with heat transmission due to stretching surface areas in production, where manufacturing process of plastic and rubber sheet through the non-functional product. Other notable applications of the study are spinning of fibers, Extrusion processes, continuous coating, and glass blowing. This was noted by some of the researchers viz., Surma Devi et al. [1] analyzed on a stretching sheet of an unsteady, 3-D boundary-layer flow. Heat and mass transfer on a stretching sheet with suction or blowing was examined by Gupta and Gupta [2], Chen and Char [3], and Vajravelu [4]. Bhattacharyya [5] shows the heat source/sink impacts of MHD flow and the transfer of heat over a shrink layer in the existence of mass suction. Jat and Chaudhary [6] investigated a stretching sheet with heat transfer on MHD flow. Fathizadeh et al. [7] have considered MHD viscous flow and heat transfer over a stretching sheet with an effective modification of the homotopy perturbation. Heat transfer over a steady stretching surface with suction was analyzed by Siri et al. [8]. Daskalakis [9] then studied free convection effects in the boundary layer along a vertically stretching flat surface. Similarity answer on MHD boundary layer across stretching surface considering thermal flux was studied by Ferdows et al. [10]. Goud and Shekar [11] have studied the effects on unsteady MHD flow past a parabolic started vertical plate with mass diffusion and viscous dissipation with variable temperature by the technique of finite element process. Wang [12] presented free convection on a perpendicular stretching surface. Bestman [13]

investigated the natural convection boundary layer in a porous medium with mass transfer and the effect of suction. Acharya et al. [14] have studied the suction and blowing effect on an acceleration surface with heat and mass transfer. An unsteady MHD flow past an impulsive inclined oscillating plate with the impact of viscous dissipation and diffusion thermo in the presence of variable temperature was deliberated by Goud and Rajahekar [15]. Ali [16] investigated the influence of suction/injection on the stretched surface power-law thermal boundary. Free convection boundary layer over a vertical porous flat plate with internal thermal generation in a permeable medium analyzed by Postelnicu et al. [17]. Shateyi [18] presented the buoyancy impacts and thermal radiation on heat & mass transfer through a semi-infinite stretching surface with suction and blowing. Chemically reactive solutions flow across the MHD boundary layer over a permissible stretching sheet with suction or blow have been explored by Bhattacharyya and Layek [19]. Goud and Rajashekar [20] presented an unsteady MHD boundary flow on the semi-infinite vertical with thermal source and suction effects via porous medium outcomes obtained by implementing the finite element method. Some researchers have studied the suction/injection and other aspects also ref. [21-29].

The current work is about an incompressible, natural convective heat transfer 3-D steady flow past on a stretching sheet involving blowing and suction. Using Boussinesq assumptions, a 3-D similarity result in the Navier-Stokes equations is reported furthermore, the current results are consistent with previously reported outcomes and seem to be a good contract in a defining context Gorla and Sidawi [30]. The governing equations are eased to a couple of non-linear ODEs that are explained using a MATLAB solver.

2. MATHEMATICAL FORMULATION

In this study, consider an incompressible, steady fluid flowing with a velocity $u=bx$ past a plane stretching perpendicular to the x -direction. Also, consider that the y -axis of the sheet makes an angle α with the horizontal and z -axis of the sheet is normal to the sheet. Components of velocity are assumed by ' u ' in the x -direction, ' v ' in the y -direction, and ' w ' in the z -direction. Figure 1 can be used as a reference for the flow model and coordinate system. Let us neglect effects along the edges and hence all the variables along the y -direction are independent. Therefore, the Boussinesq approximation governing equations are:

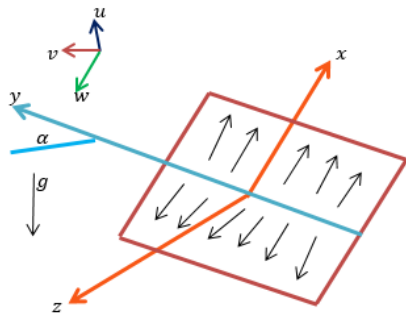


Figure 1. Scheme of a coordinate system and flow model

Momentum:

$$\frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} = 0 \quad (1)$$

$$u \frac{\partial u}{\partial x} + w \frac{\partial w}{\partial z} = g\beta(T - T_\infty)\cos\alpha + v \frac{\partial^2 u}{\partial x^2} \quad (2)$$

$$w \frac{\partial v}{\partial z} = g\beta(T - T_\infty)\sin\alpha + v \frac{\partial^2 v}{\partial z^2} \quad (3)$$

$$w \frac{\partial T}{\partial z} = -\frac{1}{\rho} \frac{\partial p}{\partial z} + v \frac{\partial^2 w}{\partial z^2} \quad (4)$$

Energy:

$$w \frac{\partial T}{\partial z} = \frac{v}{\text{Pr}} \frac{\partial^2 T}{\partial z^2} \quad (5)$$

The following are the boundary conditions to be applied:

$$\left. \begin{array}{l} u = bx, \\ v = 0, \\ w = W, \\ T = T_w \end{array} \right\} z=0 \quad ; \quad \left. \begin{array}{l} u = 0, \\ v = 0, \\ \frac{\partial w}{\partial z} = 0, \\ T = T_\infty \end{array} \right\} z \rightarrow \infty$$

3. COORDINATE TRANSFORM

When similarity solutions are used, the number of free

variables is summarized by one or more. This is the most probably used method in fluid mechanics to obtain exact solutions. Ames [31] describes the methods for equations of physical interest in generating similarity transformations. In the field of limiting solutions, asymptotic solutions are used as similarity solutions. Physical insight into these specifics of complex flows of fluid may be obtained by using similarity solutions for complex fluid flows. Most of the characteristics exhibited by these solutions describe the actual problem for the physical, dynamic, and thermal parameters.

$$\begin{aligned} u &= bx f'(\eta) + A \cos\alpha \psi(\eta), \quad v = A \sin\alpha \phi(\eta), \\ w &= -\sqrt{bv} \varphi, \quad \theta(\eta) = \frac{T - T_\infty}{T_w - T_\infty}, \\ A &= \frac{g\beta(T_w - T_\infty)}{b}, \quad \eta = \sqrt{\frac{b}{v}} \end{aligned} \quad (6)$$

The above Eq. (6) are substituted in (1)-(5) equations, then the following are the resultant equations:

$$f''' = (f')^2 - ff'' \quad (7)$$

$$\theta'' + \text{Pr} f\theta' = 0 \quad (8)$$

$$\phi'' + f\phi' + \theta = 0 \quad (9)$$

$$\psi'' + f\psi' + \theta = \psi f' \quad (10)$$

In Eqns. (7)-(8), prime refers to diff. with resp. to η only. The reduced boundary conditions for flow fields are mentioned by:

$$\left. \begin{array}{l} f(\eta) = f_w, \\ f'(\eta) = 1, \\ \theta(\eta) = 1, \\ \phi(\eta) = 0, \\ \psi(\eta) = 0 \end{array} \right\} \eta = 0 \quad ; \quad \left. \begin{array}{l} f'(\eta) = 0, \\ \theta(\eta) = 0, \\ \phi(\eta) = 0, \\ \psi(\eta) = 0 \end{array} \right\} \eta \rightarrow \infty \quad (11)$$

Here, $f_w = \frac{-W}{\sqrt{bv}}$ is the mass transfer parameter changes in a sign for injection and surjection. It is negative for injection and positive for surjection.

The stretching surface undergoes shear stresses and is given by:

$$\tau_{zx} = \mu \frac{\partial u}{\partial z} \Big|_{z=0} = \rho \sqrt{bv} [bx f''(0) + A \cos\alpha \psi'(0)] \quad (12)$$

$$\tau_{zy} = \mu \frac{\partial v}{\partial z} \Big|_{z=0} = \rho \sqrt{bv} A \sin\alpha \phi'(0) \quad (13)$$

In the direction of x and y at any point on the surface, the skin friction factors can be taken as:

$$Cf_x = \frac{2\tau_{zx}(0)}{\rho(bx)^2} = \frac{2}{\sqrt{\text{Re}_x^2}} \left(-1 + \left(\frac{\text{Gr}_x}{\text{Re}_x^2} \right) \cos\alpha \psi'(0) \right) \quad (14)$$

$$Cf_y = \frac{2\tau_{zy}(0)}{\rho(bx)^2} = \frac{2}{\sqrt{\text{Re}_x^2}} \left(\frac{Gr_x}{\text{Re}_x^2} \right) \cdot \text{Sin}\alpha \cdot \phi'(0) \quad (15)$$

where, $\text{Re}_x = \frac{(bx)x}{\nu}$, $Gr_x = \frac{x^3 g \beta (T_w - T_\infty)}{\nu^2}$. With the help of Fourier's law, the heat flux may be noted that:

$$q_w = -K_f \left(\frac{\partial T}{\partial z} \right)_{z=0} = -K_f \sqrt{\frac{b}{\nu}} (T_w - T_\infty) \theta'(0). \quad (16)$$

At any point on the surface area, the heat transfer coefficient may be noted as:

$$h = \frac{q_w}{(T_w - T_\infty)} \quad (17)$$

At any point on the surface Nusselt number be taken as:

$$Nu_L = \frac{hL}{K_f} = -\theta'(0) \cdot \sqrt{\text{Re}_L} \quad (18)$$

4. RESULTS AND DISCUSSION

This Section explains the numerical results of the set of coupled ordinary differential equations which are not linear (7)-(10) subject to the boundary conditions (11) have been executed with the aid of an in-built MATLAB numerical bvp4c problem solver for various estimations of the parameters. Heat transfer and fluid flow characteristics are numerically computed for their dependence on Prandtl number and surface mass transfer.

Table 1. With $Pr=7.0$ the outcomes of $f'(0)$, $\psi'(0)$, $\theta'(0)$, $\phi'(0)$ for different values of mass transfer factors f_w compared with ref. [30]

f_w	$f'(0)$	$\theta'(0)$	$\phi'(0)$	$\psi'(0)$
0.7	-1.418835	-5.799705	0.147772	0.142456
0.4	-1.231802	-3.989315	0.194900	0.185540
0.0	-1.014349	-1.890462	0.305539	0.281972
-0.4	-0.83420	-0.500116	0.507098	0.447013
-0.7	-0.722423	-0.087148	0.697118	0.589307

Table 2. For $f_w=0$ the different values of Pr , the outcomes of $f'(0)$, $\psi'(0)$, $\theta'(0)$, $\phi'(0)$ compared with ref. [30]

Pr	$f'(0)$	$\theta'(0)$	$\phi'(0)$	$\psi'(0)$
0.07	-1.014349	-0.352182	0.976804	0.822892
0.2	-1.014349	-0.388200	0.941902	0.795626
0.7	-1.014349	-0.534879	0.815210	0.696205
2.0	-1.014349	-0.911669	0.577967	0.507509
3.0	-1.014349	-1.159692	0.474313	0.423375
7.0	-1.014349	-1.890462	0.305539	0.281972
10	-1.014349	-2.303501	0.254389	0.237519
20	-1.014350	-3.349977	0.178888	0.170144
50	-1.014350	-5.424807	0.112816	0.109193
70	-1.014350	-6.458883	0.095310	0.092695

Wall friction and heat transfer rate causes to the varied mass transfer parameter f_w is numerically shown in Table 1. Injection increases the friction component and diminishes the

heat transfer coefficient. Alternatively, suction decreases the friction component and increases the heat transfer rate.

Increased Prandtl number extends to an increased rate of heat transfer, decreased induced buoyancy flow, and shear stress. This behavior is observed from the data in Table 2, where there are no conditions of surface mass transfer.

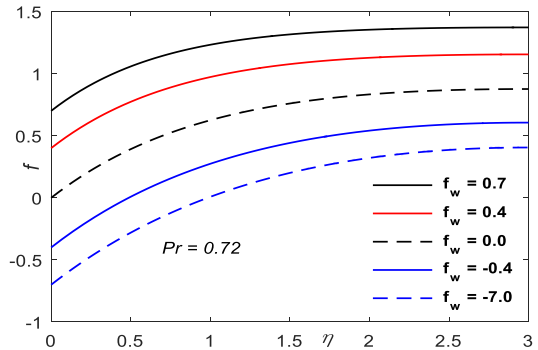


Figure 2. Stream function

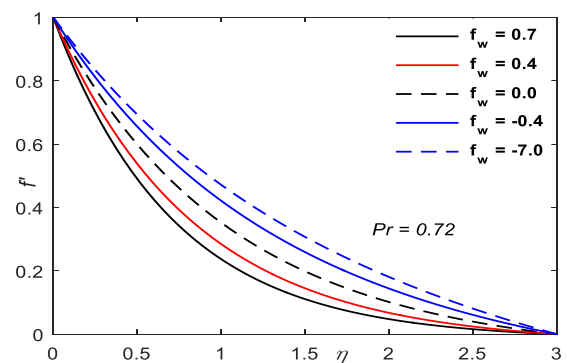


Figure 3. Within the boundary layer $f'(\eta)$ profiles (velocity in the z-direction)

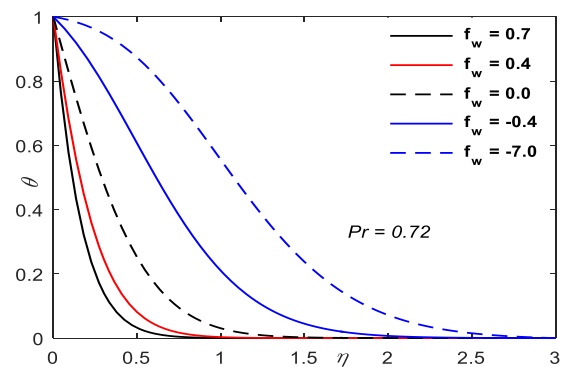


Figure 4. Temperature profiles vs f_w

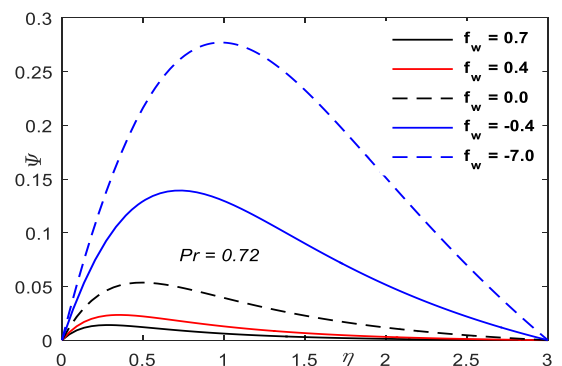


Figure 5. Velocity profiles in the z-direction

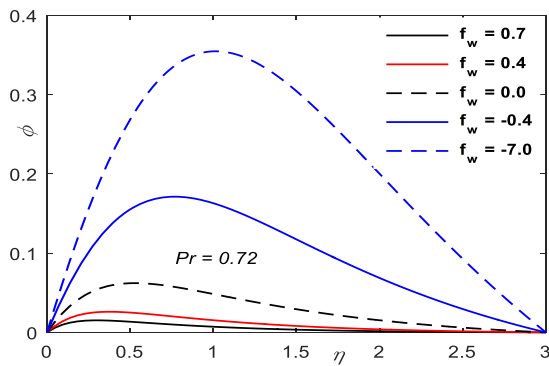


Figure 6. Velocity boundary layers in the y -direction

Figures 2 to 6 focus on the temperature and velocity distributions for the outcome of surface mass transfer. The velocity distribution component in z -direction is depicted in Figure 2 where $Pr=7.0$. There is a lot of influence on the surface mass transfer value. As that of $f'(\infty)=0$, a constant value $f(0)$ is approached $f(\eta)$ monotonically. The numerical values $f(\infty)$ are a measure of entrainment velocity. At the surface, higher entrainment velocity is due to higher suction velocity. Inside the boundary layer, $f'(\infty)$ distribution is shown in Figure 3. It can be clearly understood that a more linear shape $f'(\infty)$ is obtained by higher values of injection. The distribution of normalized temperature profiles for $Pr=7.0$ is shown in Figure 4 with varying surface mass parameter. Higher injection values, the thickness of the thermal boundary layer. Alternative behaviors of the thermal boundary layer are observed in the event of higher suction and a decrease of thermal boundary layer exponentially is observed in all specified cases. Maximum values of $\psi(\eta)$ (velocity component of z -direction of normalized free convection) and $\phi(\eta)$ (velocity component of y -direction in normalized free convection) are located far from the surface on the increasing rate of injection. Figures 5 and 6 clearly, depict the decrease of the velocity boundary layers in an exponential manner. With an increased velocity level, suction is increased. The heat flux at the surface is steep on higher values of injection. This is amalgamated with a temperature reduction at the outer boundary region. The temperature is approximately equal to the ambient temperature as length increases. In case of the rapid increase in atmospheric temperature with height, body temperature rises due to heat transfer and may not be able to achieve the local ambient temperature. When $\alpha=0$, on a vertically stretched surface, equation 14 describes a zero shear

stress $\left(\frac{Gr_x}{Re_x^2}\right)\psi'(0)=1$. Zero shear stress or critical value of the

boundary layer $\left(\frac{Gr_x}{Re_x^2}\right)$ is smaller for Prandtl numbers having

a lower value than the Prandtl numbers having higher values.

For the sample, the value $\left(\frac{Gr_x}{Re_x^2}\right)_{crit}$ is 0.1740 at $Pr=0.07$

whereas its value is 10.79 at $Pr=70$. For $\alpha \neq 0$, velocity is present in all the directions hence, on a rigid surface, there is no rise in induced natural convection in a vertical direction. Alternatively, induced natural convection is slanted in the positive direction of the y -axis, since $\phi(\eta)$ is greater than $\psi(\eta)$.

5. CONCLUSIONS

In this work, The effects of the surface mass transfer on natural convection flow from a vertical stretching surface. Tables are depicted for the missing values of thermal functions and velocity. Predictions on the rate of heat transfer can be performed using this information. Also, the surface friction factor can be estimated. The temperature field and flow field experience a higher influence by surface mass transfer. Higher entrainment velocity is observed at the surface due to suction. Linearity temperature and velocity profiles are higher with injection.

- The thickness of the thermal boundary layer is increased with an increase of injection values and alternatively reduced by surface suction as well as temperature and velocity profiles decay exponentially.
- With an increase of Pr values the result in heat transfer rate increases.
- With minor Prandtl numbers, the thermal boundary layer's thickness is found to reduce leading to reduced resistance to heat transfer.

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NOMENCLATURE

u, v, w	Velocity factors along with the x, y, z directions respectively
x, y, z	Coordinate directions
k	Thermal conductivity
Gr	Grashoff number
ω	Conditions at the surface
h	Heat transfer coefficient
Re	Reynolds number
M	Dimensionless velocity along the y -direction
N	Dimensionless velocity along the x -direction

H	Dimensionless temperature	β	Coefficient of thermal expansion
Nu	Nusselt number	μ	Viscosity
Pr	Prandtl number	η	Dimensionless distance
A	Free convection parameter	ϕ	Dimensionless velocity
T	Temperature	τ	Shear stress
ρ	Density	Cf	friction factor
g	Acceleration due to gravity	∞	Conditions far away from the surface
α	Angle		