



Distribution Law of Three Spontaneous Combustion Zones in the Goaf Area of a Fully Mechanized Working Face under High Ground Temperature

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ABSTRACT

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To figure out the distribution law of three spontaneous combustion zones in the goaf area of fully mechanized working face under high ground temperature, this study took the 11501# fully mechanized mining face of Zhujixi Coal Mine as the research object, and employed software Fluent to perform numerical simulations on the O₂ concentration distribution in the goaf; then, combining with the actual situations on the site, the high-location boreholes and grout holes of the roof gas drainage roadway of the 11501# working face were selected as measuring points to measure the O₂ concentration changes in a few positions such as in middle part of the goaf, on the air intake side, and on the air return side. The results show that, the numerical simulation results were basically consistent with the field measurement results, in the middle part of the goaf, the scope of the oxidation zone was 26.4m-62m; on the air intake side, the scope of the oxidation zone was 32m-96m; on the air return side, the scope of the oxidation zone was 28.4m-91m. The research findings of this paper provided a scientific reference for formulating fire-prevention and fire-extinguishing technical plans for mines.

1. INTRODUCTION

Coal spontaneous combustion is one of the main natural disasters in coal mines, which seriously threatens the safety of mine production [1-3]. Statistics show that among the large and medium-sized coal mines in China, mines with serious or very serious spontaneous combustion hazards account for 72.86%. According to the results of a field survey on more than 130 large and medium-sized mines in 25 major coal-producing provinces and regions in China, mines with a shortest spontaneous combustion period within 3 months account for more than 50% [4]. The spontaneous combustion of coal is also one of the main causes of coal dust and gas explosions. According to incomplete statistics, in the recent ten years, there have been 11 gas explosion accidents caused by spontaneous combustion of coal in China, resulting in 455 deaths.

Zhujixi Coal Mine is a mine with high ground pressure and high ground temperature. Mining under high ground pressure would increase the degree of coal fragmentation, thereby improving the oxidation and heat accumulation conditions [5-7]. The high ground temperature environment would inhibit convection heat loss and heat transfer of the coal, and improve the heat accumulation environment; at the same time, the high ground temperature increases the free radical activity of the coal, the oxidizability of the coal increases accordingly, and thus the risk of spontaneous combustion increases as well [8-10]. In order to study the distribution law of the three spontaneous combustion zones in the goaf area under the conditions of high ground pressure and temperature, world field scholars have carried out a lot of research, for example, through on-site observation, scholar Cheng Weimin analyzed the change laws of temperature, CO and O₂ concentration in

the goaf, and determined the scopes of the three spontaneous combustion zones according to the length of the oxidation and heat accumulation zone in the goaf [11, 12]. Scholar Zhang Xinhai established a mathematical model of seepage, oxidation, and diffusion in the goaf under drainage conditions, then he used numerical simulation to solve the model and obtained the change laws of O₂ concentration and air leakage intensity in the goaf under drainage conditions [13]. Their findings contributed a lot to the research on the three spontaneous combustion zones in the goaf, but they haven't concerned the three spontaneous combustion zones in the goaf in high ground temperature environment. Therefore, this paper takes the 11501# working face of Zhujixi Coal Mine as the research object to explore the distribution law of the three spontaneous combustion zones in the goaf under complex high ground temperature conditions, in the hopes of providing a useful reference for formulating fire-prevention and fire-extinguishing technical plans for mines.

2. DIVISION CRITERIA AND ANALYSIS OF THREE SPONTANEOUS COMBUSTION ZONES

The three spontaneous combustion zones are the heat dissipation zone, the self-ignition zone, and the suffocation zone [14-16]. As the working face of the mine is advancing, the roof of the coal seam gradually falls, forming a loose caving zone within a certain range. In this area, the heat generated by the oxidation and self-ignition of the leftover coal is mostly taken away by the air leakage, so the heat is not accumulated easily here and it won't self-ignite, and this area is called the heat dissipation zone. Then, as it goes deeper into the goaf, the air leakage becomes less and is not enough to take

away the heat generated by the oxidation of the leftover coal, the heat accumulates and the oxidation of the leftover coal accelerates, which would eventually lead to the self-ignition of the leftover coal, and this area is called the self-ignition zone. Further, in area deeper than the self-ignition zone, the speed of air leakage is smaller and the O₂ concentration is lower, which cannot support the oxidation reaction of the leftover coal, the leftover coal in this area does not have the conditions for spontaneous combustion, and this area is called the suffocation zone [17, 18].

Coal oxidation and spontaneous combustion must meet three conditions at the same time: (1) The coal has a tendency of self-ignition and is accumulated in a broken state; (2) Continuous ventilation and oxygen supply conditions; (3) Continuous heat accumulation environment, and sufficient time for oxidation. In mine goaf area with coal spontaneous combustion tendency, the volume of air leakage directly affects the oxygen supply and heat accumulation conditions of the coal, and the O₂ concentration directly determines the oxidizability of the coal seam [19-21]. Therefore, the division of the three spontaneous combustion zones in the goaf area is based on three criteria: air leakage speed, temperature distribution, and O₂ concentration [22, 23]. Among the three, the air leakage speed is a vector, which is difficult to measure; temperature is the most direct indicator reflecting the degree of spontaneous combustion of the coal, but since the coal is a poor conductor and the heat transfer process in the goaf is very complicated, the temperature changes in each zone of the goaf can hardly be measured; O₂ concentration is not only related to the air leakage state, but also related to the degree of oxidation of the leftover coal, in areas of higher degree of spontaneous combustion, the O₂ consumption is higher and the O₂ concentration is lower, the O₂ content directly reflects the oxidation and heat accumulation conditions of the leftover coal [24, 25]. Therefore, the scope of the three spontaneous combustion zones can be determined according to the distribution of O₂ concentration in the goaf; moreover, O₂ concentration is a scalar quantity, which is easy to measure on the site. In summary, the Zhujixi Coal Mine used O₂ concentration to divide the three spontaneous combustion zones in the goaf.

It is generally believed that the criteria for dividing the three spontaneous combustion zones based on O₂ concentration are: O₂ concentration of heat dissipation zone > 18%; O₂ concentration of self-ignition zone is 8%-18%; O₂ concentration of suffocation zone < 8% [26].

3. NUMERICAL SIMULATION OF THE DISTRIBUTION LAW OF O₂ CONCENTRATION IN THE GOAF

To figure out the accurate oxidation process of leftover coal in the goaf, a goaf O₂ concentration distribution law mathematical model was constructed to determine key parameters such as the permeability, O₂ consumption, and diffusion coefficient of the goaf area, and the CFD software was employed to simulate the O₂ concentration distribution law in the goaf.

3.1 Boundary conditions of the goaf model

(1) The air pressures at the intake airway and return airway were set as inlet pressure and outlet pressure, the pressure

difference was 300Pa, that is, the air pressure at the intake airway was 300Pa, and the air pressure at the return airway was 0Pa, the temperature was 300K, and the air density was 1.293kg/m³.

(2) In the construction of roof gas drainage roadway, the drainage pressure of high-location boreholes was -6kPa.

(3) In the goaf model, the upper and lower surfaces and the surrounding boundary conditions were set as Wall boundaries.

(4) The air in the roadways was compressible ideal gas, and the seepage process was regarded as a stable isothermal flow process.

(5) The air flow in the goaf conformed to the Darcy's law.

(6) The multi-medium in the goaf was regarded to be isotropic.

3.2 Determination of model parameters

According to FICK's law, the diffusion equation of various gases in the goaf is as follows:

$$J_i = \rho D_m \frac{\partial X_i}{\partial x_i} - \frac{D_i^T}{T} \frac{\partial T}{\partial x_i} \quad (1)$$

where, J_i is the diffusion flow of the i -th gas, which is mainly caused by the concentration gradient and heat gradient; ρ is the density of the mixed gas in the goaf; D_m is the diffusion coefficient of the mixed gas; X_i is the mass fraction of the i -th gas; x_i is the distance parameter; D_i^T is the heat diffusion coefficient; T is temperature.

For non-rarefied gases, Formula (1) can be replaced by the form of multi-component diffusion, namely:

$$J_i = \rho \frac{M_i}{M_{mix}} \sum_{j, j \neq i} D_{ij} \left(\frac{\partial X_j}{\partial x_i} + \frac{X_j}{M_{mix}} \frac{\partial M_{mix}}{\partial x_i} \right) - \frac{D_i^T}{T} \frac{\partial T}{\partial x_i} \quad (2)$$

where, M_i is the relative molecular weight of gas i ; M_{mix} is the relative molecular weight of the mixed gas; D_{ij} is the multi-component diffusion coefficient of component i in gas j .

The physical adsorption, chemical adsorption, and coal-oxygen recombination processes between oxygen and leftover coal are the main reasons for the continuous decrease in O₂ concentration in the goaf. The O₂ consumption rate in the low-temperature oxidation stage is:

$$R_{O_2} = AV_{O_2}^n \exp(-E/RT) \quad (3)$$

where, E is the activation energy of the reaction, its value varies between 12-95kJ/mol according to the different coal types, in this experiment, its value takes 62 kJ/mol; A is the pre-exponential factor, which depends on the coal rank and the test method; n is a constant, its value is between 0.5-1.0; R is the gas constant; R_{O_2} is the volume fraction of O₂.

3.3 Determination of danger zone in the goaf

The physical parameters of the 11501# fully mechanized mining face are as follows: the strike direction length of the goaf was 145m, the dip direction length of the goaf was 220m, the roadway section was 5.2m×4m, the working face section was 7.2m×2m, the model height was 50m, the coal seams extended in the horizontal direction and were upward mined at 2~9°, U-shaped ventilation mode was adopted, and the air

volume distribution of the working face was 1670m³/min.

3.4 Numerical simulation results

Based on above parameters, the Fluent software was employed to perform numerical simulations on the O₂ concentration in the goaf, and the results are shown in Figure 1. The O₂ concentration in the middle of the goaf decreased with the increase of the distance from the working face. When the distance from the working surface was 26.2m, the O₂ concentration dropped to 18%; when the distance from the working surface reached 62.5m, the O₂ concentration dropped to 8%. The air leakage on the air intake side was stronger, the

decline trend of O₂ concentration was slower, when the distance from the working face was 31.5m, the O₂ concentration dropped to 18%; when the distance from the working face was 96.2m, the O₂ concentration dropped to 8%, and it entered the suffocation zone. As for the air return side, under the impact of the drainage of high-location boreholes, the air leakage was stronger, the decline trend of O₂ concentration was slower, when the distance from the working face was 28.2m, the O₂ concentration dropped to 18%; when the distance from the working face was 90.6m, the O₂ concentration dropped to 8%, and it entered the suffocation zone.

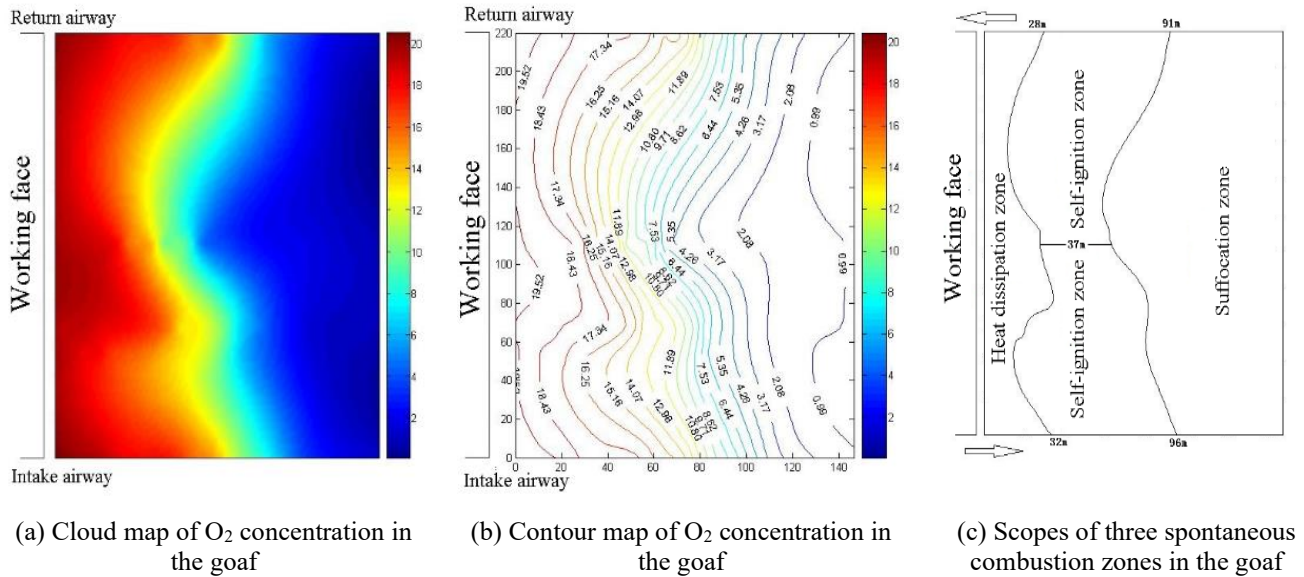


Figure 1. Cloud and contour maps of O₂ concentration in the goaf and the scopes of three spontaneous combustion zones

4. FIELD MEASUREMENT

4.1 Overview of the working face

Zhujixi Coal Mine is a coal and gas outburst mine. The 11₂ coal seam was first mined as the lower protective layer of the 13₁ coal. The 11₂ coal that was mined first was identified as an outburst coal seam with a maximum original gas pressure of 1.2MPa and a maximum original gas content of 8.63m³/t, its shortest spontaneous ignition period is 45 days, and it belongs to the Type II spontaneous combustion coal seam, the coal dust has the risk of explosion.

The 11501# working face that was first mined is located in the 5-th mining area of the 11₂ coal, which has the characteristics of deep burial and high ground temperature, the burial depth of the coal seam is 744.17-1108.88m, and the surrounding rock temperature is 35.44-46.56°C. In the working face, the occurrence of coal seam is stable with an average thickness of 1.59m. The working face is 220m wide, the stoping length is 1480m, and the roof gas drainage roadway is 64.2m staggered along the track roadway of the working face. At 1.8-8.7m in the upper part of the 11₂ coal seam of the working face is the 11₃ coal, the thickness of the 11₃ coal seam is 0.35m, it falls into the goaf area with the stoping of the working face, and the 11₂ coal that has not been fully stoped when the working face crosses the fault becomes the leftover coal, which has increased the leftover coal in the goaf. At the same time, the gas drainage increases the air

leakage of the goaf, creating conditions for the spontaneous combustion of leftover coal in the goaf.

4.2 Layout of measuring points

Making use of the high-location boreholes and the grout holes of the roof gas drainage roadway of the 11501# working face, four measuring points were arranged near the positions of the intake airway, the middle part of the goaf, and the return airway to observe the change laws of O₂ concentration in the goaf, the layout of the measuring points is shown in Figure 2.

When the measuring points entered the goaf area, the measurement started and the gas composition was analyzed by a gas chromatograph. After analyzing the data, the change curves of O₂ concentration in the goaf with the advancing distance of the working face were plotted, as shown in Figure 3.

According to Figure 3, the O₂ concentration in the middle part of the goaf of the 11501# mining face decreased rapidly with the advancement of the working face. When the depth of the goaf reached 26.4m, O₂ concentration dropped to 18%, and when the depth of the goaf reached 62m, O₂ concentration dropped to 8%, and it entered the suffocation zone. The air leakage on the air intake side was stronger, the O₂ concentration decreased slowly, when the depth of the goaf reached 32m, O₂ concentration dropped to 18%, when the depth of the goaf reached 96m, O₂ concentration dropped to 8% and it entered the suffocation zone. On the air return side,

under the impact of the drainage of high-location boreholes, the air leakage was stronger, the O₂ concentration decreased slowly, when the depth of the goaf reached 28.4m, O₂ concentration dropped to 18%, when the depth of the goaf reached 91m, O₂ concentration dropped to 8% and it entered the suffocation zone.

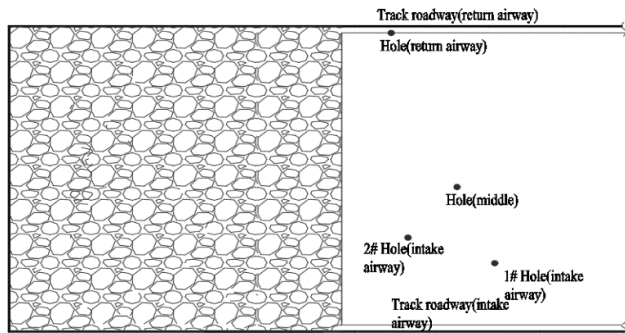


Figure 2. Layout of measuring points

Based on the simulation results, the field measurement results of O₂ concentration, and the division criteria, the scopes of the three spontaneous combustion zones in the goaf of the 11501# fully mechanized mining face were obtained, as listed in Table 1.

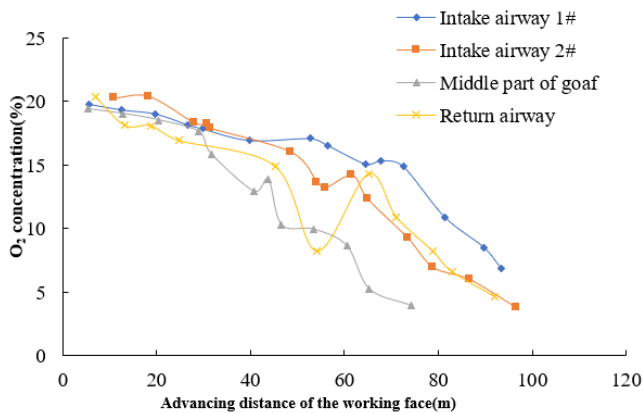


Figure 3. Change curves of O₂ concentration in the goaf with the advancing distance of the working face

Table 1. Scopes of the three spontaneous combustion zones in the goaf divided based on O₂ concentration

Position	Scope of the heat dissipation zone (m)	Scope of the self-ignition zone (m)	Scope of the suffocation zone (m)
On the air intake side	<32	32-96	>96
In the middle of the goaf	<26.4	26.4-62	>62
On the air return side	< 28.4	28.4-91	> 91

5. CONCLUSIONS

(1) According to the actual conditions of the 11501# fully mechanized mining face, the Fluent software was employed to perform numerical simulations on the O₂ concentration in the goaf area. The results showed that, in the middle part of the

goaf, when the distance from the working face was 26.2m, the O₂ concentration dropped to 18%; when the distance from the working face reached 62.5m, the O₂ concentration dropped to 8%. On the air intake side, when the distance from the working surface was 31.5m, the O₂ concentration dropped to 18%; when the distance from the working surface was 96.2m, the O₂ concentration dropped to 8%. On the air return side, when the distance from the working surface was 28.2m, the O₂ concentration dropped to 18%; when the distance from the working surface was 90.6m, the O₂ concentration dropped to 8%.

(2) A few measuring points were arranged on site to measure the O₂ concentration in the goaf area of the 11501# working face, and the obtained results showed that, in the middle part of the goaf, when the depth of the goaf was 26.4m, the O₂ concentration dropped to 18%; when the depth of the goaf was 62m, the O₂ concentration dropped to 8%. On the air intake side, when the depth of the goaf reached 32m, the O₂ concentration dropped to 18%; when the depth of the goaf reached 96m, the O₂ concentration dropped to 8%. On the air return side, when the depth of the goaf reached 28.4m, the O₂ concentration dropped to 18%; when the depth of the goaf reached 91m, it dropped to 8%.

(3) The numerical simulation results and the field measurement results were basically the same. The scope of the oxidation zone in the goaf area was 26.4m-62m; on the air intake side, its scope was 32m-96m; on the air return side, its scope was 28.4m-91m.

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