Thermodynamic performance analysis and simulation test of composite thermal insulation wall

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ABSTRACT

Buildings accounts for more than 25% of the total energy consumption of our society, calling for better building energy-saving measures to improve the insulation performance of building walls. This paper explores the thermodynamic parameters (e.g. temperature field and temperature stress) of building thermal insulation wall. Firstly, the variation law of the temperature field of the building wall was simulated under the condition of external insulation structure; on this basis, the external insulation structure was compared with the internal insulation structure in terms of temperature stress variation. The research conclusions are as follows: The insulation materials in the wall significantly reduced the energy exchange between the indoor and outdoor environments. Under intense solar radiation, the surface temperature of the external wall was mainly affected by solar radiation; under weak solar radiation, the surface temperature of the external wall was mainly affected by the ambient temperature. Owing to the insulation layer, the temperature on the inner surface of the wall changed far slower than the external wall temperature. The temperature varied insignificantly from the surface of the inner wall to the inner surface of insulation layer, but significantly within the insulation layer. In the external insulation wall, the outermost decorative surface and the crack-resistant mortar layer both had a small temperature difference between the inner surface and the outer surface, witnessed a negative correlation between the surface temperature and temperature stress, and suffered mainly from tensile stress. Under significant variation of the ambient temperature, the two layers are likely to crack under the huge stresses. In winter, the base layer of the external insulation structure mainly suffered from compressive stress, while that of the internal insulation structure from tensile stress. In general, the external insulation structure can better protect the structural layer of the wall than the internal insulation structure; on this basis, the external insulation structure was compared with the internal insulation structure in terms of temperature stress variation. The research findings lay a theoretical basis for the engineering application of the building wall insulation technology (BWIT) and shed new light on the prevention of wall durability problems (e.g. cracking and breaking) caused by temperature stress changes.

1. INTRODUCTION

Statistics show that buildings accounts for more than 25% of the total energy consumption of our society. This calls for better building energy-saving measures to improve the insulation performance of building walls [1-2].

Building wall insulation technology (BWIT) has become the main means of building energy conservation, thanks to its convenience and low cost in construction [3]. The BWIT adds energy-saving thermal insulation materials into the wall maintenance structure to save energy by controlling the energy transfer between the inside and outside of the building [4-5]. The latest thermal insulation wall mainly consists of such three parts as the base layer, the thermal insulation layer and the additional layer. Among them, the thermal insulation layer is the core to building energy conservation. It is usually made of materials like polystyrene board, polystyrene or aerated concrete [6-9].

Depending on the construction method, the BWIT can be divided into the external insulation technology of outer wall, the internal insulation technology of outer wall and the sandwich insulation technology [10-12]. The external insulation technology of outer wall is the most widely used construction method. However, the insulation layer is prone to cracking and aging in the service period because the insulation layer lies outside the base layer. The internal insulation technology of outer wall also has many defects, such as occupying indoor area and proneness to cold bridges and condensation [13-16].

To solve the above problems, this paper explores the thermodynamic parameters (e.g. temperature field and temperature stress) of building thermal insulation wall. Firstly, the variation law of the temperature field of the building wall was simulated under the condition of external insulation structure; on this basis, the external insulation structure was compared with the internal insulation structure in terms of temperature stress variation. The research findings lay a theoretical basis for the engineering application of the BWIT and shed new light on the prevention of wall durability problems (e.g. cracking and breaking) caused by temperature stress changes.
2. THERMODYNAMIC MODEL OF TEMPERATURE FIELD IN BUILDING INSULATION WALL AND ANALYSIS OF CALCULATION RESULTS

2.1 Building wall structure and initial parameters

Figure 1 shows a typical external insulation structure of building wall as well as the width and materials of each layer. The period change of the external air temperature $T_a$ can be calculated as:

$$T_a = -\sin\left(\frac{2\pi(t + 2)}{24}\right) \left(\frac{T_{\text{max}} - T_{\text{min}}}{2}\right) + \left(\frac{T_{\text{max}} + T_{\text{min}}}{2}\right)$$

where $T_{\text{max}}$ and $T_{\text{min}}$ are the daily maximum and minimum temperatures, respectively.

![External insulation structure of building wall](image)

Figure 1. External insulation structure of building wall

2.2 Mathematical model of building wall temperature field

For simplicity, the building wall was considered as a mean structure, and the thermal resistance between the layers in Figure 1 was neglected. Then, the temperature at any position $(x, y, z)$ in the wall can be expressed as:

$$\frac{\partial T}{\partial t} = \frac{\lambda}{\varphi} \left(\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2}\right)$$

where $\lambda$ and $c$ are the thermal conductivity and the specific heat of the material, respectively. According to the actual test results, the temperature of the wall varies very slightly in the length $x$ and width $y$ directions. Hence, equation (2) can be normally simplified as:

$$\frac{\partial T}{\partial t} = \frac{\lambda}{\varphi} \frac{\partial^2 T}{\partial z^2}$$

Then, the mathematical model of building wall temperature field can be set up with the following parameters: the indoor air temperature $T_{\text{in}}$, the inner wall surface temperature $T_{\text{i}}$, the indoor heat exchange coefficient $\beta_{\text{in}}$. Thus, the heat exchange amount $q_{\text{in}}$ between the inner wall surface and the indoor can be expressed as:

$$q_{\text{in}} = \beta_{\text{in}} [T_{\text{in}}(t) - T_{\text{i}}(t)]$$

Similarly, the heat exchange amount $q_{\text{out}}$ between the outer wall and the outdoor can be expressed as:

$$q_{\text{out}} = \beta_{\text{out}} [T_{\text{out}}(t) - T_a(t)]$$

The solar radiation on the outer wall surface is subjected to the following boundary condition:

$$q_r = \alpha_s I_r$$

2.3 Calculation results and analysis

Figure 2 presents the winter temperature changes in the building walls with south-facing and north-facing external insulation structures, respectively. As shown in Figure 2, the indoor temperature changed periodically, but by a small amplitude (<3℃); the insulation materials in the wall significantly reduced the energy exchange between the indoor and outdoor environments; the ambient air has a major impact on the temperature of the outside wall surface, as evidenced by the greater-than-12℃ temperature difference between the outer surface of the insulation layer and the outer surface of the south-facing wall.

![Winter temperature changes in the building walls](image)

Figure 2. The winter temperature changes in the building walls with south-facing and north-facing external insulation structures
Figure 3 shows the winter temperature changes in the building walls with south-facing and north-facing external insulation structures, respectively, under solar radiation. From Figures 2 and 3, it can be seen that the outer wall surface was warmer than the ambient air under solar radiation. When the solar radiation intensity was weak, the temperature of the outer wall started to decrease gradually, but with a certain delay compared with the variation in solar radiation intensity. The wall surface temperature was affected by different factors in different cases. Under intense solar radiation, the surface temperature of the external wall was mainly affected by solar radiation; under weak solar radiation, the surface temperature of the external wall was mainly affected by the ambient temperature. Owing to the insulation layer, the temperature on the inner surface of the wall changed far slower than the external wall temperature.

The solar radiation also has a significant impact on the temperature field of the building wall. As shown in Figures 2 and 3, the peak temperature of the south-facing wall stood at 13°C, towering over that of the north-facing wall (3.5°C), for the north-facing wall is less exposed to solar radiation than the south-facing wall. For both walls, the minimum temperature was around -11°C. In addition, the maximum temperature difference of the south-facing wall reached 24°C.

![Figure 3](image1)

Figure 3. The winter temperature changes in the building walls with south-facing and north-facing external insulation structures under solar radiation.

![Figure 4](image2)

Figure 4. Winter temperature distribution of the wall in the thickness direction

The winter temperature distribution of the wall in the thickness direction is shown in Figure 4, where the origin O is the inner surface temperature of the wall and the x-axis is the distance from the inner surface. Obvious, the temperature decreased very slowly from the inner wall surface indoor to the inner surface of the insulation layer, plunged rapidly in the insulation layer, and plummeted by nearly 30°C at the surface of the outer wall. This means the external insulation can effectively suppress the escape of indoor energy, making the base wall more stable and durable.

3. ANALYSIS OF TEMPERATURE STRESS VARIATION IN BUILDING INSULATION WALL

3.1 Mathematical model of temperature stress

Based on the above analysis, this section further investigates the temperature stress variation in building insulation wall. Equation (3) was simplified to express temperature field function T as a function of time $t$ and wall thickness:

$$T = f(t, z)$$  \hspace{1cm} (7)

Since the temperature stress is negligible in the length and width of the wall, this paper only considers the temperature stress variation in the thickness direction. After the addition of the insulation layer, the wall is composed of multiple layers of materials. Thus, the strain $\varepsilon$ of each layer under the effect of temperature stress can be expressed as:

$$\varepsilon_1(z) = \alpha_1(A_1 + B_1z_1)$$
$$\varepsilon_2(z) = \alpha_2(A_2 + B_2z_2)$$
$$\varepsilon_3(z) = \alpha_3(A_3 + B_3z_3)$$
$$\vdots$$
$$\varepsilon_n(z) = \alpha_n(A_n + B_nz_n)$$  \hspace{1cm} (8)
The parameters A and B can be derived from the following formulas:

\[
A_i = \frac{1}{h_i} \int \frac{d_1}{2} [T_i(z_i) - T_{i0}] \, dz_i
\]

\[
B_i = \frac{1}{h_i} \int \frac{d_1}{2} [T_i(z_i) - T_{i0}] \, dz_i
\]

\[
A_n = \frac{1}{h_n} \int \frac{d_n}{2} [T_n(z_n) - T_{n0}] \, dz_n
\]

\[
B_n = \frac{1}{h_n} \int \frac{d_n}{2} [T_n(z_n) - T_{n0}] \, dz_n
\]

Then, the temperature stress \( \sigma_{iT} \) of the i-th layer material under full constraints is:

\[
\sigma_{iT} = -\frac{E_i \alpha_i (T_i - T_{i0})}{1-\mu} \quad (10)
\]

The temperature stress \( \sigma_{i1} \) of the i-th layer material under mean temperature is:

\[
\sigma_{i1} = -\frac{E_i \alpha_i}{1-\mu} A_i \quad (11)
\]

The temperature stress \( \sigma_{i2} \) of the i-th layer material under linear temperature is:

\[
\sigma_{i2} = -\frac{E_i \alpha_i}{1-\mu} B_i z_i \quad (12)
\]

Considering the actual constraints of the wall, the temperature stress can be discussed in the following two cases:

Case 1: The wall is unconstrained, i.e. the freeform condition:

\[
\sigma_i = \sigma_{i3} = \sigma_{iT} - \sigma_{i1} - \sigma_{i2} \quad (13)
\]

Case 2: The wall is fully constrained:

\[
\sigma_i = \sigma_{iT} \quad (14)
\]

The building insulation structure can be generally divided into the structural layer (reinforced concrete blocks) and the additional layer (insulation layer and protective structure). The additional layer, mainly anchored or pasted to the structural layer, has poor mechanical properties and often deforms simultaneously with the structural layer.

3.2 Analysis of calculated temperature stress

The temperature stresses of the external insulation and internal insulation walls were calculated based on the results of the temperature field acquired in the previous section. The first step is to analyze the situation that the insulation layer is outside the base wall. Figure 5 displays the temperature stress variation in the outermost decorative surface of the external insulation wall.

It can be seen that the outermost decorative surface had a small temperature difference between the inner surface and the outer surface, indicating that the temperature-induced bending stress was relatively small. When the wall was unconstrained, the temperature stress was basically zero, revealing that the temperature of the decorative layer obeyed a linear distribution. In addition, the surface temperature of the decorative layer is inversely proportional to the temperature stress, and the maximum temperature corresponds to the minimum temperature stress; the inverse is also true. In winter, the decorative surface was mainly subjected to tensile stress, which peaked at 0.55MPa. The stress varied in a range smaller than 0.5MPa. Thus, the decorative surface is prone to cracking in winter.

Figure 5. The temperature stress variation in the outermost decorative surface of the external insulation wall

Figure 6 illustrates the temperature stress variation of the crack-resistant mortar layer in the external insulation wall.

Figure 6. The temperature stress variation in the crack-resistant mortar layer of the external insulation wall
can be seen that the crack-resistant mortar layer also had a small temperature difference between the inner surface and the outer surface, indicating that the temperature-induced bending stress was relatively small. When the wall was unconstrained, the temperature stress was basically zero, revealing that the temperature of the decorative layer obeyed a linear distribution. In winter, the crack-resistant mortar layer was mainly subjected to tensile stress, which peaked at 0.4 MPa. The variation of stress was controlled within 0.4 MPa.

Figure 7 exhibits the temperature stress variation in the base layer of the external insulation wall. As shown in the figure, there was a certain difference between the inner and outer surfaces of the base layer, revealing a major impact of temperature on the bending stress of the base layer. When the wall was unconstrained, the temperature stress stood at zero, a sign of the small heat exchange between indoor and outdoor. The base layer was mainly subjected to compressive stress.

4. CONCLUSIONS

This paper explores the thermodynamic parameters (e.g. temperature field and temperature stress) of building thermal insulation wall. Firstly, the variation law of the temperature field of the building wall was simulated under the condition of external insulation structure; on this basis, the external insulation structure was compared with the internal insulation
structure in terms of temperature stress variation. The research conclusions are as follows:

(1) The insulation materials in the wall significantly reduced the energy exchange between the indoor and outdoor environments. Under intense solar radiation, the surface temperature of the external wall was mainly affected by solar radiation; under weak solar radiation, the surface temperature of the external wall was mainly affected by the ambient temperature. Owing to the insulation layer, the temperature on the inner surface of the wall changed far slower than the external wall temperature. The temperature varied insignificantly from the surface of the inner wall to the inner surface of insulation layer, but significantly within the insulation layer. The external insulation can effectively suppress the escape of indoor energy, making the base wall more stable and durable.

(2) In the external insulation wall, the outermost decorative surface and the crack-resistant mortar layer both had a small temperature difference between the inner surface and the outer surface, witnessed a negative correlation between the surface temperature and temperature stress, and suffered mainly from tensile stress. Under significant variation of the ambient temperature, the two layers are likely to crack under the huge stresses. In winter, the base layer of the external insulation structure mainly suffered from compressive stress, while that of the internal insulation structure from tensile stress. In general, the external insulation structure can better protect the structural layer of the wall than the internal insulation structure.

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