

SEMICONDUCTOR, MOLECULAR CRYSTALS AND OXIDE TEMPERATURE PRESSURE OPHASE DIAGRAM

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ABSTRACT

The melting temperature-pressure phase diagram [T_m(P)-P] for semiconductor, molecular crystals and oxide are predicted through the Clapeyron equation where the pressure-dependent volume difference is modeled by introducing the effect of surface stress induced pressure. Semiconductor, molecular crystals and oxide have been employed to test the reliability of the model, because of its important role. For Si and Ge, the stable state under normal pressure is the diamond structure (Si-I and Ge-I). Through pressure, this change in the diamond structure for beta -Sn structure (Si-II and Ge-II), and with the increase of temperature, phase I and II are going to be melting into a liquid (L). For the CO₂ crystal (commonly known as dry ice), it is a molecular solid with a structure of Pa3 at low temperature and low pressure (CO₂-I), and can be widely used for cooling. Al₂O₃ has been extensively investigated because of its widely ranging industrial applications. This includes applications as a refractory material both of high hardness and stability up to high temperatures, as a support matrix in catalysis. MgO is a material of key importance to earth sciences and solid-state physics: it is one of the most abundant minerals in the Earth and a prototype material for a large group of ionic oxides.

Keywords: Phase transitions, Pressure-dependent, Temperature, Oxides.

1. INTRODUCTION

High pressure research is a powerful tool to explore key and electronic states of nature in solids. Due to high pressure often produce a lot of new structure in the elements or compounds, so it has become a significant change in a way of atomic distance and coordination number. With the development of high pressure research unceasingly thorough, the temperature pressure phase diagram (T/P) caused by theoretical and experimental home interest. In recent years, the generation and measurement of simultaneous high pressures and high temperatures has undergone rapid development with the diamond anvil cell (DAC) technique [1-4]. We choose Si, Ge, CO₂, Al₂O₃ and MgO to verify the reliability of the model, because, although the T-P phase diagram of this substances have been obtained through the experiments is established, but the measurement accuracy under high temperature and pressure is not high, so most of the phase diagram are experimental, or is the schematic, the existing data has not been confirmed theoretically. Therefore, more in-depth theoretical work is necessary.

For Si and Ge, as everyone knows, the steady state under normal pressure is the diamond structure (Si-I and Ge-I). Through pressure, this change in the diamond structure for beta -Sn structure (Si-II and Ge-II), and with the increase of temperature, phase I and II will melt, into a liquid (L). For the CO₂ crystal (commonly known as dry ice), it is a molecular solid with a structure of Pa3 at low temperature and low pressure (CO₂-I), and can be widely used for cooling.

As the pressure increases, several high pressure phases appeared, including the P4₂/mmn symmetric structure (CO₂-II), Cmca orthorhombic structure (CO₂-III), the structure of Pbcn (CO₂-IV) and polymerization of the quartz structure (CO₂-V) etc. However, for this high pressure phase is still uncertain, especially have yet to determine precisely their stable field. Al₂O₃ and MgO have been employed to test the reliability of the model, because of its important role. Al₂O₃ has been extensively investigated because of its widely ranging industrial applications. This includes applications as a refractory material both of high hardness and stability up to high temperatures, as a support matrix in catalysis, as well as a variety of fundamental interests [5-8]. MgO is a material of key importance to earth sciences and solid-state physics: it is one of the most abundant minerals in the Earth (especially its lower mantle) and a prototype material for a large group of ionic oxides. The classic Clapeyron equation governing all first-order phase transitions of pure substances may be useful to determine the T_m (P)-P curve theoretically in the following form [9],

$$dp = \frac{\Delta H(T_m, P)}{\Delta V(T_m, P)T_m} dT_m \quad (1)$$

where H (T_m,P) show the gram-atom melting enthalpy and V(T_m,P) is gram-atom volume change during the melting with Δ denoting the change. Eq. (1) can describe the joint rate of change dP/dT_m along the phase equilibrium lines and

estimate the derived properties of ΔH and ΔV . To utilize Eq. (1) for determination of phase diagram, a $T_m(P)$ function or an integration of Eq. (1) is needed. Since both $\Delta H(T_m, P)$ and $\Delta V(T_m, P)$ are functions of temperature and pressure, and the necessary separation of variables cannot be accomplished in any direct and known manner, the integration of Eq. (1) has been carried out through approximate methods ever since the equation was first established in the 19th century [9]. Although when $\Delta P = P - P_0$ and $\Delta T = T_m - T_{m0}$ are small, $\Delta H(T_m, P) \approx \Delta H(T_{m0}, P_0)$ and $\Delta V(T_m, P) \approx \Delta V(T_{m0}, P_0)$ have minor error where the subscript 0 denotes the initial points and Δ denotes the difference [6], as ΔP and ΔT increase, exact functions of $\Delta H(T_m, P)$ and $\Delta V(T_m, P)$ must be known [9]. Thus, a successful application of Clapeyron equation for $T_m(P)$ -P phase diagram depends on establishing accurate $\Delta H(T_m, P)$ and $\Delta V(T_m, P)$ functions.

Recently, a general equation without any free parameter for surface stress f has been established as follows [10],

$$f(T_{m0}) = (h/2)[3\Delta S_{vib}\Delta H_{m0}/(\kappa_S V_S R)]^{1/2} \quad (2)$$

where h is atomic diameter, ΔS_{vib} is the vibrational part of the overall melting entropy ΔS_m , $S_m = S_{el} + S_{pos} + S_{vib}$, S_{el} is negligibly small, and $S_{pos} = -R[x_A \ln(x_A) + x_v \ln(x_v)]$, where $x_A = 1/(1 + \Delta V_m)$ and $x_v = \Delta V_m / (1 + \Delta V_m)$ are the molar fractions of the host material and vacancies, respectively [11], for oxides $\Delta S_{vib} \approx \Delta S_m - \Delta S_{pos}$, $\kappa = -\Delta V / (V_P)$ is compressibility of the crystal, V_S is gram-atom volume of crystals, R shows the ideal gas constant and ΔH_{m0} is bulk melting enthalpy at T_{m0} .

The predicted f values of various materials in terms of Eq. (2) are in agreement with the known experimental and theoretical results obtained from the first principle and the classic mechanics calculations [10]. Since the measured thermodynamic amounts in Eq. (2) has reflected usually unknown surface states of materials [10], Eq. (2) supplies an easy way to establish a relationship between the surface stress induced internal pressure P_i for small particles and T_m , which brings out a possibility to determine $\Delta V(T_m, P)$ function.

$\Delta H_m(T_m)$ function can be determined by Helmholtz function, $\Delta H_m(T_m) = \Delta G_m(T_m) - T_m d\Delta G_m(T_m)/dT_m$, where $\Delta G_m(T_m)$ denotes the temperature dependent solid-liquid Gibbs free energy difference. For oxides, $\Delta G_m(T_m) = \Delta H_{m0} T_m (T_{m0} - T_m) / T_{m0}^2$ where ΔH_{m0} is the melting enthalpy at the melting temperature T_{m0} [12]. This function was modeled by treating $\Delta H_m(T_m)$ to be a linear function where the heat capacity difference ΔC_p between crystal and liquid to be a constant. Using a mathematic approximation that the quantity $\ln(T_{m0}/T_m)$ is approximately equal to $2(T_{m0} - T_m)/(T_{m0} + T_m)$ with neglecting of higher order terms. Thus,

$$\Delta H_m(T_m) = \Delta H_m(T_m/T_{m0})^2. \quad (3)$$

In this contribution, through assuming that $\Delta V(T_m, P)$ and $\Delta H(T_m, P)$ functions may be determined by Eqs. (2) and (3), $T_m(P)$ curves are obtained with an integration of Clapeyron equation when suitable original points for each integration are selected. It is found that the model prediction of the $T_m(P)$ -P phase diagram of corundum is consistent with the experimental results and other theoretical predictions [16-18].

2. MODEL

To find a solution of Clapeyron equation, as a first order approximation, $\Delta H_m(T_m, P) \approx \Delta H_m(T)$ and $\Delta V_m(T_m, P) \approx \Delta V_m(P)$ are assumed [9], which lead to a simplification of Eq. (1),

$$dP = \frac{\Delta H_m(T_m)}{\Delta V_m(P) T_m} dT_m. \quad (4)$$

$\Delta V_m(P) = (V_L - V_S) + (\Delta V_L - \Delta V_S)$ where the subscripts S and L denote solid and liquid, respectively. $\Delta V_S = -V_S P_S \kappa_S$ and $\Delta V_L = -V_L P_L \kappa_L$ where V_L and V_S are known data. To find a solution of the equation, a relationship between P_L and P_S must be found. To do that, a spherical particle with a diameter D is considered. In light of the Laplace-Young equation, $P_S = 4f/D$ and $P_L = 4\gamma/D$ where γ is the surface energy of the liquid [10]. Thus, $\Delta V_L = -V_L P_S (\gamma/f) \kappa_L$ because $P_S/P_L = f/\gamma$. Substituting this relationship into $\Delta V_m(P)$ function,

$$\Delta V_m(P) = V_L - V_S + [V_S \kappa_S - V_L (\gamma/f) \kappa_L] P \quad (5)$$

where P_S has been simplified as P . when the initial point of (P_0, T_0) is selected as $(0, T_{m0})$ where T_{m0} is the melting temperature under ambient pressure, integrating Eq. (5) with $\Delta H_m(T_m)$ and $\Delta V_m(P)$ functions in terms of Eqs. (3) and (5),

$$\int_0^P \{V_L - V_S + [V_S \kappa_S - V_L (\gamma/f) \kappa_L] P\} dP = (\Delta H_{m0} / T_{m0}^2) \int_{T_{m0}}^{T_m} T_m dT_m,$$

or

$$T_m(P) = T_{m0} \sqrt{1 + \{2(V_L - V_S)P + [V_S \kappa_S - V_L (\gamma/f) \kappa_L] P^2\} / \Delta H_{m0}} \quad (6)$$

Although the above discussion on P is related with the surface stress induced internal pressure P_i for a spherical particle, they may be extended to a general case for the pressure effect on T_m , which is illustrated as follows: Let P denote the sum of P_i and the external pressure P_e , namely [16],

$$P = P_i + P_e. \quad (7)$$

When $P_e \approx 0$, $P = P_i$. This is the case of the size-dependent melting. When $P_i \approx 0$ with $D \rightarrow \infty$, $P = P_e$, which is the usual situation of the pressure-dependent melting for bulk materials. Since any pressure source should have the same effect on materials properties, P_i can be substituted by P_e . Thus, although P denotes P_i in above $T_m(P)$ equation, it has been considered as P_e and is simplified as P .

3. RESULTS AND DISCUSSION

Figs.1 and Figs.2 describes the melting curve on the Si T-P phase diagram and Si nano crystals and T-P phase diagram of Ge according to equation (6) compared model predicted results and experimental results and other theoretical results, parameters used are listed in Table. 1. Figure. 1 present a

comparison for T-P phase diagram of bulk Si and the melting curve of Si nanocrystal among the model predictions and experimental and other theoretical results. The solid lines denote model predictions in terms of Eqs. (6) Where necessary parameters used are listed in Table .1. The symbols \circ , \square , Δ show experimental results. The dash and dot lines denote other theoretical results. Other symbols denote I-II transition pressure at room temperature where n denotes the theoretical result, $+$ denotes the experimental results under non-hydrostatic pressure, \blacklozenge , \diamond and ∇ denote the experimental results under hydrostatic pressure. For the melting of Si nanocrystal, the two dash lines show the predicted results where the corresponding T_{ml} (D) values denoted as \times (1478 K) and \blacktriangle (1371 K) are obtained from other theoretical result and Eq. (6), respectively. For comparison, the dot line gives the theoretical result for melting of Si nanocrystal. Figs.1 and Figs.2 in the P-T relationship is through the small particles produced by internal pressure considered and applied in bulk crystals of external pressure equivalent to the idea of the establishment of the. However, equation (6) limit the size of nano crystal used in P_i must be taken into account; it is equal to $6h$. For the I-L transformation, the corresponding $6hI = 1.4112$ nm, according to $PI = 4 f$ more I/D , we obtain the limit pressure for the $PI = 10.5$ GPa. while at $PI < P < Pt$ this pressure range, the error of P-T curve and the experimental results of our model predicted only small, but this will still give the triple point (Pt determination of Tt), bring some inaccuracy. In order to improve the accuracy and the experimental results more in line with that, we take the approach in determining $P > PI$ curve is: the curve tangent direction line extend along at $P = 10.5$ GPa place, this is because the experimental results confirm the pressure is large enough melting curve is approximately a straight line. Similarly, for the transformation of the Ge I-L, when $6hI = 1.47$ nm, $PI = 6.12$ GPa. We have taken and the Si class Like the way to deal with $PI < P < Pt$ the range of pressure curve. For the T-P phase diagram of Si and Ge, I-II phase boundary shift is very fuzzy, change the pressure distribution in the reported a wide range, especially at low temperatures, and change due to the very slow lag. As shown in the figure, although we chose different experimental results at room temperature with a mean value of $PI-II$ to determine the transition curve of I-II, but the results of model predictions and the experimental results are in good agreement, this shows that the average results of the phase boundary of this transition and

experiment is very close to the. In fact, our model predicted results and experimental results or have a certain error, this may be caused because we neglected the effect of compression of the pressure coefficient.

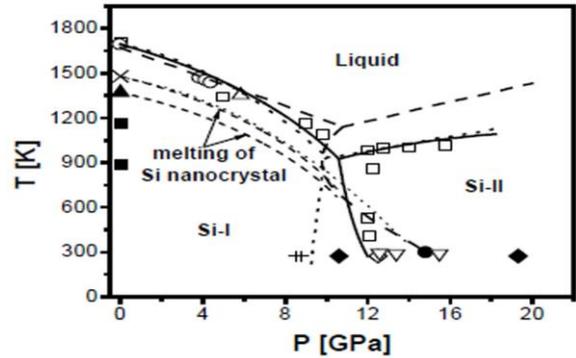


Figure 1. A comparison for T-P phase diagram of bulk Si and the melting curve of Si nanocrystal among the model predictions and experimental and other the oretical results

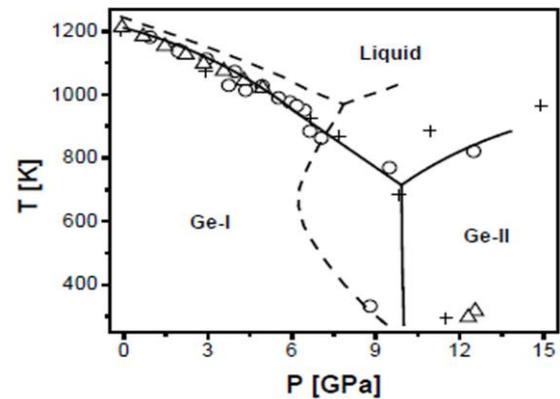


Figure 2. A comparison for T-P phase diagram of bulk Ge among the model predictions and experimental and other theoretical results

The solid lines denote model predictions in terms of Eqs. (6) where necessary parameters used are listed in Table 1. The symbols Δ , $+$ and O show experimental results. The dash lines denote other theoretical results.

Table 1. Necessary parameters for calculating T-P phase diagram of Si and Ge and the melting curve of Si nanocrystals in terms of Eqs. (6)

	I-L transition		I-II transition		II-L transition			
	Si	Ge	Si	Ge	Si	Ge		
T_{ml}	1693	1210.4	T_{I-II}^d	273	273	T_I^f	960	714
			P_{I-II}^d	12	10	P_I^f	11.6	9.915
V_I^a	12.06	13.64	V_I^a	11.00	11.93	V_{II}^a	8.53	9.66
V_L^a	10.93	12.94	V_{II}^a	8.53	9.66	V_L^a	10.93	12.94
κ_I^b	1.02	1.33				κ_{II}^b	0.885	1.19
κ_L	10.00	10.00				κ_L	10.00	10.00
f_I^c	3.707	2.252				f_{II}^c	2.797	1.589
γ	0.765	0.581				γ	0.765	0.581
ΔH_{I-L}	50.55	36.94	ΔH_{I-II}^e	0.78	0.2	ΔH_{II-L}^e	53.67	37.74

Fig.3 A comparison for TI-L(P) curve of bulk CO₂-I between the model prediction and experimental results. The solid line denotes the model prediction in terms of Eqs. (6) where necessary parameters used are: $T_{mi} = 215.55$ K, $V_L = M/\rho_L = 12.43$ cm³·g-atom⁻¹ with $M = 14.67$ g·g-atom⁻¹ and $\rho_L = 1.18$ g·cm⁻³, $V_I = 10.65$ cm³·g-atom⁻¹, $\kappa_I = 1/BI = 8.06 \times 10^{-11}$ Pa⁻¹ with $BI = 12.4$ GPa, $\kappa_L \approx 100 \times 10^{-11}$ Pa⁻¹ as a first order approximation is equal to the κ_L value of CS₂ since CS₂ as a linear molecule has a similar behavior of CO₂, $\Delta H_{I-L} = 2.649$ KJ·g-atom⁻¹, $\gamma = 0.00913$ J·m⁻², and $fI = 0.5613$ J·m⁻² is calculated by Eq.(6) with $hI = (2^{1/2}/2)a_1 = 0.3575$ nm where $a_1 = 0.5056$ nm for Pa³ structure and $\Delta S_{vib}^{I-L} = 8.856$ J·g-atom⁻¹·K⁻¹. The dot lines show the experimental phase diagram.

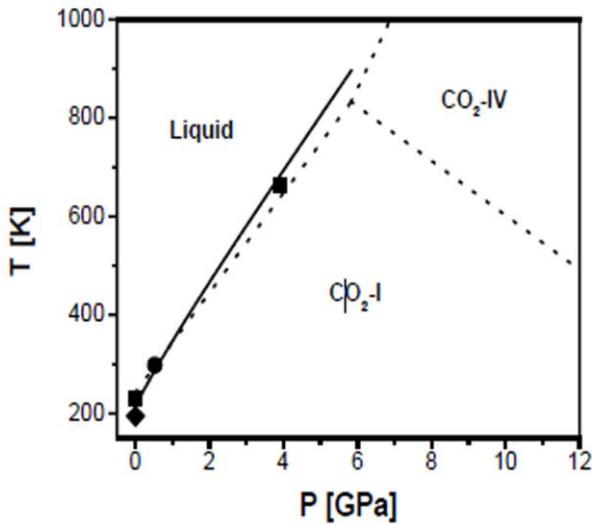


Figure 3. A comparison for TI-L(P) curve of bulk CO₂-I between the model prediction and experimental results

Figure.4 presents comparison between the model predictions of Eq. (6) and experimental result of pressure dependent melting of Al₂O₃. As shown in the figure, T_m increases as P increases. This is evidently induced by positive volume change ΔV during the melting. Thus, However, the low size limit of nanocrystals for the application of P_i in Eq. (6) must be considered, a crystal is characterized by its long-range order and the smallest nanocrystal should have at least a half of the atoms located within the particle [17]. Hence, the smallest D_{min} is $2D_0$. For Al₂O₃, $D_{min} = 1.146$ nm in term of $D_0 = 3h$ for nanocrystals [7]. The curvature-induced pressure P approximately equals to 20.10 GPa by Laplace-Young equation $P_i = 4f/D$ associated with Eq. (2). The value of T_m on the melting curve $T_m(P)$ must be determined. As shown in the figure, Clapeyron equation, without any adjustable parameter, is consistent with the experimental result and other theoretical prediction [13-15]. The $T_m(P)$ - P relationship in Figs. 1 is made by a generalization where the internal pressure of small particles is considered to be equivalent to that of the bulk one.

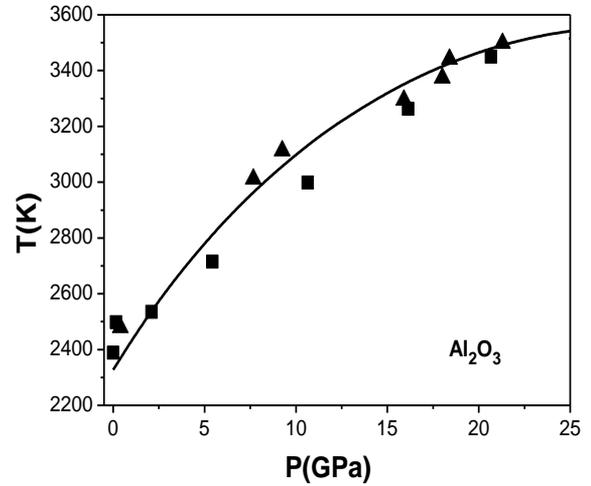


Figure 4. Presents comparison between the model predictions of Eq. (6) and experimental result of pressure dependent melting of Al₂O₃

Figs.5 presents comparison between the model predictions of Eq. (6) and experimental result of pressure dependent melting of MgO. As shown in the figure, T_m increases as P increases. This is evidently induced by positive volume change ΔV during the melting. Thus, However, the low size limit of nanocrystals for the application of P_i in Eq. (6) must be considered, a crystal is characterized by its long-range order and the smallest nanocrystal should have at least a half of the atoms located within the particle [17]. Hence, the smallest D_{min} is $2D_0$. For MgO, $D_{min} = 1.284$ nm in term of $D_0 = 3h$ for nanocrystals. The curvature-induced pressure P approximately equals to 25.39 GPa by Laplace-Young equation $P_i = 4f/D$ associated with Eq. (2). The value of T_m on the melting curve $T_m(P)$ must be determined. As shown in the figure, Clapeyron equation, without any adjustable parameter, is consistent with the experimental result and other theoretical prediction. The $T_m(P)$ - P relationship in Figs.2 is made by a generalization where the internal pressure of small particles is considered to be equivalent to that of the bulk one.

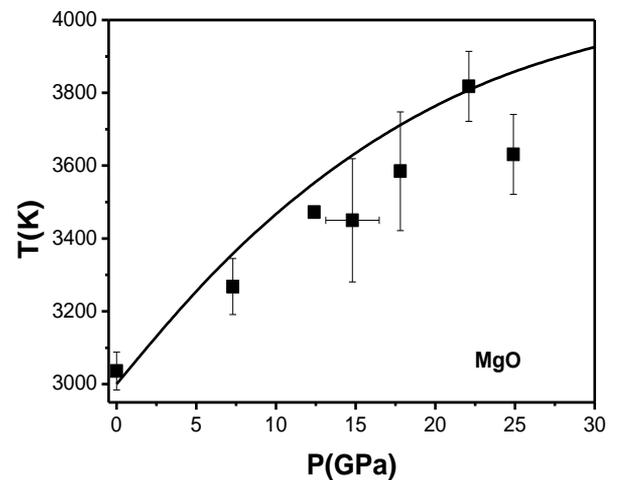


Figure 5. Presents comparison between the model predictions of Eq. (6) and experimental result of pressure dependent melting of MgO

Since Clapeyron equation may govern all first-order phase transitions, the above consideration may be generalized for different phase transitions. Moreover, the success of Eq. (6) implies that the both assumptions of essentially ΔH_m being a function of temperature and ΔV_m being a function of pressure are reasonable.

4. CAPTIONS

Fig.1 A comparison for T-P phase diagram of bulk Si and the melting curve of Si nanocrystal among the model predictions and experimental and other theoretical results. The solid lines denote model predictions in terms of Eqs. (6) where necessary parameters used are listed in Table.1. The dash and dot lines denote other theoretical results. Other symbols denote I-II transition pressure at room temperature where n denotes the theoretical result, + denotes the experimental results under non-hydrostatic pressure, \blacklozenge , \diamond and ∇ denote the experimental results under hydrostatic pressure. For the melting of Si nanocrystal, the two dash lines show the predicted results where the corresponding $T_m(I(D))$ values denoted as \times (1478 K)

and \blacktriangle (1371 K) are obtained from other theoretical result and Eq. (6), respectively. For comparison, the dot line gives the theoretical result for melting of Si nanocrystal.

Figure. 2 A comparison for T-P phase diagram of bulk Ge among the model predictions and experimental and other theoretical results. The solid lines denote model predictions in terms of Eqs. (6) where necessary parameters used are listed in Table.1. The symbols Δ , + and O show experimental results. The dash lines denote other theoretical results.

Figure. 3 A comparison for TI-L(P) curve of bulk CO₂-I between the model prediction and experimental results. The solid line denotes the model prediction in terms of Eqs. (6) where necessary parameters used are: $T_{mI} = 215.55$ K, $V_L = M/\rho_L = 12.43$ cm³· g-atom⁻¹ with $M = 14.67$ g· g-atom⁻¹ and $\rho_L = 1.18$ g· cm⁻³, $V_I = 10.65$ cm³· g-atom⁻¹, $\kappa_I = 1/BI = 8.06 \times 10^{-11}$ Pa⁻¹ with $BI = 12.4$ GPa, $\kappa_L \approx 100 \times 10^{-11}$ Pa⁻¹ as a first order approximation is equal to the κ_L value of CS₂ since CS₂ as a linear molecule has a similar behavior of CO₂, $\Delta H_{I-L} = 2.649$ KJ· g-atom⁻¹, $\gamma = 0.00913$ J· m⁻², and $fI = 0.5613$ J· m⁻² is calculated by Eq.(6) with $hI = (2I/2)aI = 0.3575$ nm where $aI = 0.5056$ nm for Pa3 structure and $\Delta S_{vib-I-L} = 8.856$ J· g-atom⁻¹· K⁻¹. The dot lines show the experimental phase diagram.

Figure. 4 The pressure-temperature melting diagram of Al₂O₃, where the solid line shoes the model prediction of Eq. (6). The theoretical and experimental results are also plotted in the figure. The symbols \blacksquare and \blacktriangle denote the theoretical estimations and the experimental observations [13]. The necessary parameters in Eq. (6) are as follows: $T_m = 2327$ K [18], $H_m = 21.76$ KJ g-atom⁻¹[19], $S_m = H_m/T_m = 9.35$ Jg-atom⁻¹K⁻¹, $S_m = S_{el} + S_{pos} + S_{vib}$, S_{el} is negligibly small, and $S_{pos} = -R[x_A \ln(x_A) + x_V \ln(x_V)]$, where $x_A = 1/(1 + \Delta V_m)$ and $x_V = \Delta V_m / (1 + \Delta V_m)$ are the molar fractions of the host material and vacancies, respectively [20], and ΔV_m is the volume difference between the crystal and corresponding fluid at T_m . As result, $S_{vib} = S_m - S_{pos}$ or $S_{vib} \approx S_m + R[x_A \ln(x_A) + x_V \ln(x_V)]$

[21]. $\Delta V_m = (V_L - V_S)/V_S$, $S_{vib} = 5.6$ Jg-atom⁻¹K⁻¹, $h = 0.191$ nm [18], $\gamma = 0.690$ Jm⁻², $\kappa_S = 3.86 \times 10^{-12}$ Pa⁻¹ is determined by $\kappa = 1/B$ with $B = 289.55$ GPa being the bulk modulus [21], $V_S = 5.14$ cm³ g-atom [21], $V_L = 6.16$ cm³g-atom⁻¹ [18], $\kappa_L = 57.9 \times 10^{-12}$ Pa⁻¹ as a first-order approximation under higher pressure, we assume $\kappa_L \approx 15\kappa_S$ [13]. f is calculated through Eq. (2) and $f = 4.5$ Jm⁻².

5. CONCLUSION

In summary, we have demonstrated the reliability of simple thermodynamic model in calculating the high pressure melting of solid by comparisons between obtained melting temperature and experimental melting data for Al₂O₃ and MgO. It is found that the model predictions are consistent with the present experimental and theoretical results. Since the Clapeyron equation may govern all first-order phase transitions, the Clapeyron equation supplies a new way to determine the T-P phase diagram of materials.

ACKNOWLEDGMENT

This work was supported by Science and technology project of Jilin province education department during the Twelfth Five-year Plan Period (No.2013232).

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